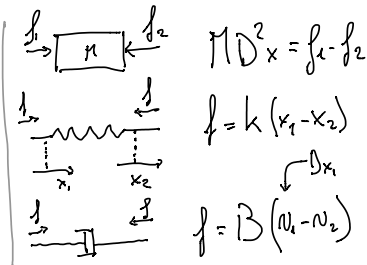


MODELLISTICA

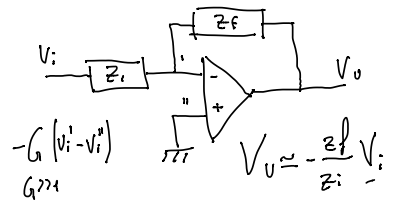
—W— $V = Ri$

—1— $v = \frac{1}{C} \int i(t) dt \Rightarrow D_{NC} = \frac{i}{C}$

—m— $v = L Di$



OPERAZ. CON BIPOLI



LAPLACE

$$F(s) = \int_0^{\infty} f(t) e^{-st} dt$$

$$\mathcal{L}[Df] = sF(s) - f(0^+)$$

$$\mathcal{L}[D^i f] = s^i F(s) - \sum_{j=0}^{i-1} s^j D^{i-j-1} f_+$$

$$\mathcal{L}\left[\int_0^t f(\omega) d\omega\right] = \frac{1}{s} F(s)$$

VALORE FINALE, INIZIALE

$$\lim_{t \rightarrow \infty} f = \lim_{s \rightarrow 0} sF \quad \lim_{t \rightarrow 0^+} f = \lim_{s \rightarrow \infty} sF$$

TRASLAZIONE TEMPO, S

$$\mathcal{L}[f(t-t_0) \cdot 1(t-t_0)] = F \cdot e^{-ts}$$

$$\mathcal{L}[f e^{at}] = F(s-a)$$

NOTEVOLI

$$\mathcal{L}[t^n] = \frac{n!}{s^{n+1}} \quad \mathcal{L}[e^{at}] = \frac{1}{s-a}$$

FATTI SEMPLICI

$$F(s) = \frac{b(s)}{(s-p_1)(s-p_2)\dots} \rightarrow \frac{k_1}{(s-p_1)} + \frac{k_2}{(s-p_2)} + \dots$$

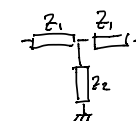
$$k_i s = \frac{1}{(j-1)!} D^{j-1} [(s-p_i)^j F] \Big|_{s=p_i}$$

$$\mathcal{L}^{-1}\left[\frac{k}{s-p} + \frac{\bar{k}}{s-\bar{p}}\right] = 2|k| e^{\alpha t} \cos(\gamma t + \arg k)$$

$$\mathcal{L}^{-1}\left[\frac{1}{(s-a)^n}\right] = \frac{1}{(n-1)!} t^{n-1} e^{at}$$

$$\mathcal{L}[1(t)] = \frac{1}{s} \quad \mathcal{L}[t^n 1(t)] = \frac{n!}{s^{n+1}}$$

TEGPOLO



$$Z = Z_1 + Z_2 + \frac{Z_1 \cdot Z_2}{Z_2}$$

DERIVATE GENERALIZZ.

$$f = g + (f_1 - f_2) \cdot 1$$

$$D^* f = Df + (f_1 - f_2) \delta$$

$$D^{**} f = D^2 f + (D^{**} f_1 - D^{**} f_2) \delta + \dots + (f_1 - f_2) \delta^{(n-1)}$$

$$\left\{ \begin{array}{l} c_{-1} + c_0 \delta + c_1 \delta^{(1)} + \dots \\ d_{-1} + d_0 \delta + d_1 \delta^{(1)} + \dots \end{array} \right\} \leftarrow \begin{array}{l} \text{COND. INIZIALI} \\ \text{DISTRIBUZIONE} \end{array}$$

$$\sum_{i=1}^n a_i D^i y = \sum_{i=1}^m b_i D^i u$$

FUNZIONI TRASF.

$$\sum_{i=1}^n a_i D^i y = \sum_{i=1}^m b_i D^i u$$

$$Y = \frac{\sum_{i=1}^n b_i s^i}{\sum_{i=1}^m a_i s^i} U + \dots$$

$$Y = G \cdot U \leftarrow \begin{array}{l} \text{ZSP} \\ \text{SISTEMA} \end{array} \quad \text{guadagno} \rightarrow k = \frac{b_0}{a_0}$$

$$\text{polinomio} \rightarrow \sum_{i=1}^n a_i s^i \quad \text{condizioni} \rightarrow g_s(t) \leftarrow \begin{array}{l} \text{ZSP} \\ \text{SISTEMA} \end{array}$$

$$\text{mod.} \rightarrow e^{pt}, t e^{pt} \dots$$

VASCHY

$$y_{\text{fine}}(t) = \int_0^t u(\omega) g_s(t-\omega) d\omega + u(0^+) g_s(t) = g_s \mu$$

SISTEMI DINAMICI PRIMO ORD.

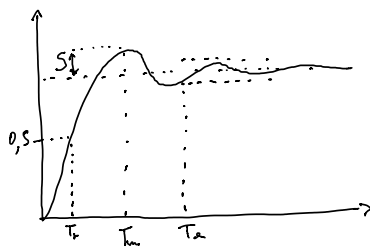
$$G(s) = \frac{1}{1 + \tau s}$$

$\tau = \text{cost. } s: \text{ tempo}$

RISP. A GRADINO

$$1 - e^{-t/\tau} \quad t \geq 0$$

$$t = 3\tau \Rightarrow 95\%$$



PER SISTEMI DI ORDINE SUP.
SI APPROSSIMA CON POLI DOM.

$\rightarrow$ COMPLESSI CONIUGATI $\rightarrow$ ORDINE 2

SIST. DIN. SECONDO ORD.

$$G(s) = \frac{\omega_n^2}{s^2 + 2\delta\omega_n s + \omega_n^2}$$

$\omega_n \rightarrow$ pulsazione naturale

$\delta \rightarrow$ coeff. smorzamento

POLI: $-\delta\omega_n \pm j\omega_n\sqrt{1-\delta^2}$

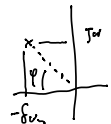
MODI: $e^{-\delta\omega_n t} \sin(\omega_n\sqrt{1-\delta^2} t + \varphi_1)$

RISP. GRADINO

$$1 - A e^{-\delta\omega_n t} \sin(\omega_n\sqrt{1-\delta^2} t + \varphi)$$

$$\frac{1}{\sqrt{1-\delta^2}}$$

$$\arctan \frac{\sqrt{1-\delta^2}}{\delta}$$



$$S = 100 \exp\left\{-\frac{\delta\pi}{\sqrt{1-\delta^2}}\right\} \quad T_d \approx \frac{3}{\delta\omega_n} \quad T_s \approx \frac{1.8}{\omega_n}$$

STABILITÀ

$\rightarrow$ Stabile se nessun polo a parte reale positiva

$\rightarrow$ Asintot. se nessun polo su asse $j\omega$

$\rightarrow$ Instabile se polo puramente $j\omega$ con moltep > 1

$\rightarrow$ BIBO $\rightarrow$ azione forzante limitata $\Rightarrow$ risp. forzata limitata

BIBO $\Leftrightarrow$ ASINT. STABILE



STABILE



INSTABILE



ASINT. STABILE

EQ. CARATTERISTICA

$$a_n s^n + \dots + a_0 = 0 \quad \leftarrow 1 + L(s)$$

SINGOLARITÀ ROUTH

$\rightarrow$ PRIMO ELEMENTO NULLO

$p =$ numero di zeri

moltiplica per $(-1)^p$ e trasla verso sx di p post:

$\rightarrow$ POLI SOMMA A ULTIMA RIGA

$\rightarrow$ TUTTI ELEMENTI NULLI

bisogna trarre polinomio ausiliario

$$\beta(s) = \gamma_{n-2i,1} s^{2i} + \gamma_{n-2i,2} s^{2i-2} + \dots \rightarrow \beta(s) = 0 \rightarrow \text{DERIVA}$$

CRITERIO ROUTH

n	$\swarrow \searrow$		
$\vdots$			
0			

$$\gamma_{k,j} = -\frac{\begin{vmatrix} \gamma_{n-2,1} & \gamma_{n-2,j+1} \\ \gamma_{k-1,1} & \gamma_{k-1,j+1} \end{vmatrix}}{\gamma_{k-1,1}}$$

PRIMA COLONNA

$\rightarrow$ VARIAZIONE $\Rightarrow R_1^+$ $\rightarrow$ INSTABILE

$\rightarrow$ PERMANENZA $\Rightarrow R_2^-$

POSSIBILE MOLTIPLICARE PER k

COEFF. SOSTITUISCONO GLI ZERI NELLA TABELLA DI ROUTH

PERMANENZE =

RADICI PURAMENTE IMMAGINARIE

DIAGRAMMI BODE

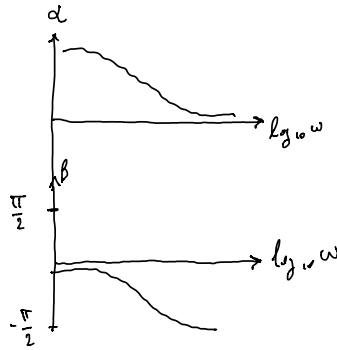
$$F(\omega) = G(j\omega)$$

$$\text{AMPIEZZE} \rightarrow \alpha = \lg_{10} |G(j\omega)|$$

$$\text{FASI} \rightarrow \beta = \arg(G(j\omega))$$

→ SI POSSONO SOMMARE

IN CATENA I DIAGRAMMI



FORME STANDARD

$$k_1 \frac{s^h + b_{n-1}s^{n-1} + \dots + b_0}{s^h + a_{n-1}s^{n-1} + \dots + a_0}$$

$$k_1 \frac{(s-z_1)(s-z_2)\dots}{(s-p_1)(s-p_2)\dots}$$

costante di trasferimento

PULSAZIONE RISONANTE

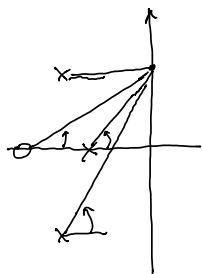
$$\omega_R = \arg \max |G(j\omega)|$$

$$\text{PICO} \rightarrow M_R = |G(j\omega_R)|$$

$$k \frac{(1+\tau_1's)(1+\tau_2's)\dots \left(1+2\delta_1 \frac{s}{\omega_{n1}} + \frac{s^2}{\omega_{n1}^2}\right)\dots}{s^h (1+\tau_1's)(1+\tau_2's)\dots}$$

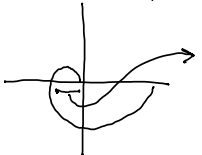
h = 0	TIPO ZERO
1	TIPO UNO
2	TIPO DUE

DIAGRAMMI NYQUIST



$$\arg = \sum \angle z - \sum \angle p$$

$k_1 > 0$



- per fase π
- tra ω

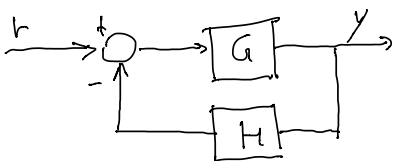
TIPO 0 → parte da punto su asse reale

TIPO 1 → asintoto

$$\sigma_a = k_1 \frac{a_1 b_1 - a_2 b_0}{a_1^2}$$

$$= k \left[\sum \tau_i' - \sum \tau_i + \underbrace{\sum 2 \frac{\delta_i'}{\omega_{n1}^2} - \sum 2 \frac{\delta_i}{\omega_{n1}^2}}_{\text{CORR. CONTINUA}} \right]$$

SISTEMI RETROAZIONATI

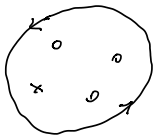


$$T_{ry} = \frac{G}{1+GH}$$

$L = GH$

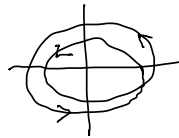
STABILE $\Leftrightarrow$ RADICI $1+L(s)$
PARTE RE NEGATIVA

TEOR. INDICE LOG.



GIRI CURVA
IMMAGINE
ANTI-ORARIO
ATTORNO ORIGINI
 $= N_z - N_p$

$\mathbb{C}_+$ SEMIPIANO
POSITIVO



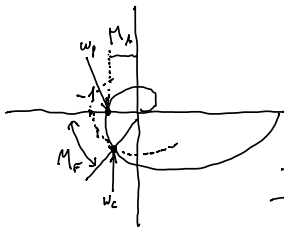
CRITERIO NYQUIST

SIST ASINTOTICAM. STABILE
 $\rightarrow$ diag. polo non tocca -1
lo circonda $\curvearrowright$ tante volte
quanti: sono i poli in $\mathbb{C}_+$

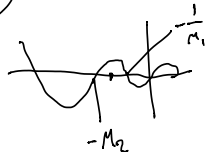
CASO PARTICOLARE

$\rightarrow$ se non ci sono poli in $\mathbb{C}_+$ allora
non deve toccare né circondare -1

MARGINI STABILITÀ



$$M_{A/B} \in (1, +\infty) = 20 \log M_A$$



$$M_A = \min \{M_1, M_2\}$$

$$M_F = \min \{\phi_1, \phi_2\}$$

LUOGO RADICI

- tanti zeri quanti sono i poli
- zeri: attirano i poli
- mantenere simmetria asse reale
- poli si respingono tra di loro
- sempre complessi coniugati

FA PARTE LUOGO
DIRETTO $\rightarrow$ PUNTO CHE A D
K > 0 HA NUMERO DISPARI
POLI E ZERI

K < 0 $\rightarrow$ PARI

INTERSEZIONE ASINTOTI

$$\sigma_a = \frac{\sum p_i - \sum z_i}{n - m} \leftarrow \text{ASCISSA}$$

$$\varphi_{a,v} = \frac{(2v+1)\pi}{n-m} \quad v=0, 1, \dots, n-m-1 \leftarrow \text{ANGOLI}$$

ANGOLO PARTENZA

$$\varphi = \pi + \sum_{k=0}^n \angle (p_i - z_k) - \sum_{i=1}^m \angle (p_i - p_j)$$

↑
K > 0
altrementi
non c'è

PER ANGOLI DI ARRIVO
SI SOSTITUISCE Z: A P:

RADICE DEL LUOGO CON MOLTIPLICITÀ H
 $\rightarrow$ PUNTO IN COMUNE A H RAMI
 $\rightarrow$ H RAMI ENTRANTI, H USCENTI
 $\rightarrow$ DIVIDONO LO SPAZIO IN
SETTORI π/H

$\frac{P}{n}$
NUMERO
ASINTOTI



DIRETTO

K > 0

p=1

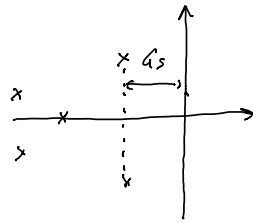
p=2

p=3

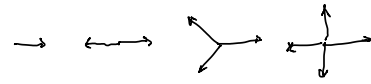
p=4

GRADO STABILITÀ

$$G_S = -\max\{R_{e p_1}, R_{e p_2}, \dots\}$$



INVERSO $K < 0$

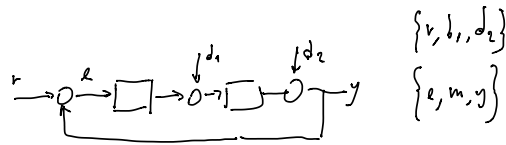


SE $\exists$ COPPIA DOMINANTE

$$\tau_s \approx \frac{3}{G_S}$$

PROGETTO SISTEMA RETROAZIONE

Sistema asintoticamente e internamente stabile
quando tutte FDE per ingressi e uscite sono
asint. stabili



SIST. STABILE SSE

- RADICI PARTE REALE NEGATIVA
- CANCELLAZ. POLO-ZERO IN C^-

$$S = T_{re} = \frac{1}{1+L} \quad T_{ry} = 1-S$$

SENSITIVITÀ

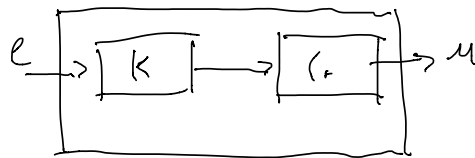
ORDINI CONTROLLORI

0: $C(s) = k$

1: $C(s) = \frac{b_1 s + b_0}{s + a_0}$

2: $C(s) = \frac{b_2 s^2 + b_1 s + b_0}{s^2 + a_1 s + a_0}$

definiti: mediante parametrizzazione
funzione d: trasferimento



INTEGRATRICE

$$C_r = \frac{1}{1+\tau s} \quad \tau > 0$$

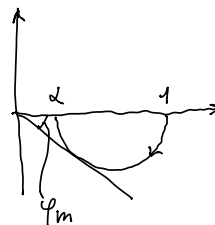
DERIVATRICE

$$C_r = \frac{\tau s}{1+\tau s} \quad \tau > 0$$

→ AZIONE COMPENSATRICE
→ FORMULE INVERSIONE

RITARATRICE

$$C_r = \frac{1+\alpha \tau s}{1+\tau s} \quad \alpha \in (0,1) \quad \tau > 0$$

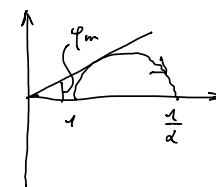


$$\varphi_m = -\arcsin \frac{1-\alpha}{1+\alpha}$$

$$\omega_m = \frac{1}{\sqrt{\alpha} \cdot \tau}$$

ANTICIPATRICE

$$C_r = \frac{1+\tau s}{1+\alpha \tau s} \quad \alpha \in (0,1) \quad \tau > 0$$



$$\varphi_m = \arcsin \frac{1-\alpha}{1+\alpha}$$

→ esempio corretto in zotale

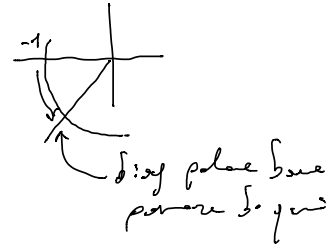
FORMULE INVERSIONE

$$M_{\varphi} = \frac{1+\beta \alpha}{1+\beta \alpha \kappa}$$

$$M = \frac{\sqrt{1+(\tau \omega)^2}}{\sqrt{1+(\alpha \tau \omega)^2}}$$

$$\begin{cases} \alpha = \frac{M \cos \varphi - 1}{M(M - \cos \varphi)} \\ x = \frac{M - \cos \varphi}{\sin \varphi} = \tau \omega \end{cases} \quad \varphi = \operatorname{atg}(\tau \omega) - \operatorname{atg}(\alpha \tau \omega)$$

MARGINE FASE



RETE ANTICIPATRICE M_F

→ SECUEN ω_0 AFFINCHÉ

$$\varphi_0 := M_F - \operatorname{arg} L(j\omega_0) - \pi$$

$$\cos \varphi_0 > |L(j\omega_0)|$$

$$M_i = \frac{1}{|L(j\omega_0)|} \quad \varphi = \varphi_0$$

RETE RETARDATRICE M_F

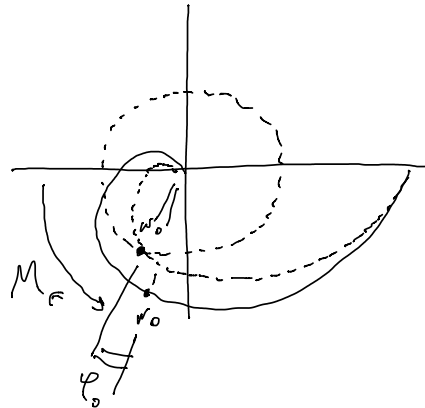
→ SECUEN ω_0 AFFINCHÉ

$$\varphi_0 := \operatorname{arg} L(j\omega) + \pi - M_F$$

$$\cos \varphi_0 > \frac{1}{|L(j\omega_0)|}$$

$$M := |L(j\omega_0)| \quad \varphi = \varphi_0$$

→ τ, α



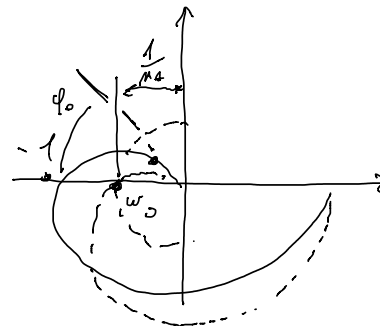
RETE ANTICIPATRICE M_A

→ ω_0 AFFINCHÉ

$$\varphi_0 = -\operatorname{arg} L(j\omega_0) - \pi$$

$$\cos \varphi_0 > M_A |L(j\omega_0)|$$

$$M := \frac{1}{M_A |L(j\omega_0)|} \quad \varphi = \varphi_0$$



RETE RETARDATRICE M_A

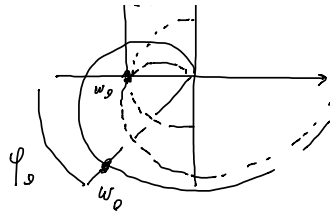
→ ω_0 AFFINCHÉ



$$\varphi_0 = \arg L(j\omega_0) + \pi$$

$$\cos \varphi_0 > \frac{1}{M_0 |L(j\omega_0)|}$$

$$M := M_0 |L(j\omega_0)| \quad \varphi = \varphi_0$$



→ OMISIIIS RBTI T, AR, DIÖFANTEA ETC...

CONTROLLO DIGITALE

CAMPIONAMENTO SHANNON

SPETTRO UNITARIO $0 - \omega_s$

PULSARE - CAMPIONAMENTO

RICOSTRUZIONE DA $\tilde{f}(k) = f(kT)$

$\Leftrightarrow$

$$\Omega = 2\pi/T \geq 2\omega_s$$

TRASF. Z

$$\mathcal{Z}[x(k)] = \sum_{k=0}^{\infty} x(k) z^{-k} \quad \text{ver. amplice}$$

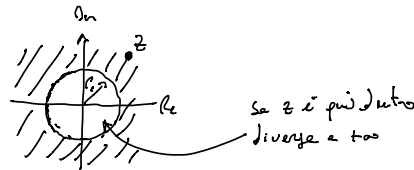
||

$$X(z) = x(0) + x(1)z^{-1} + \dots$$

La serie è convergente nella regione ROC

$$\left\{ \sum_{k=0}^{\infty} x(k) z^{-k} < \infty \right\} \rightarrow |z| > \rho_c$$

↑
raggio assoluto
convergenza



se z è più dentro
diverge a ∞

SEGNALE RITARDATO N PASSI

ARTICOLI - $\dots - i - (i) z^{n-i}$

$$\mathcal{Z}[x(k-n)] = z^{-n} \mathcal{Z}[x(k)] + \sum_{k=0}^{n-1} x(k-n) z^{-k}$$

→ caso in cui n è nullo

$$\mathcal{Z}[x(k-n)] = z^{-n} X(z)$$

$$\mathcal{Z}[a^k x(k)] = X\left(\frac{z}{a}\right)$$

VALORE INIZIALE

$$x(0) = \lim_{z \rightarrow \infty} X$$

VALORE FINALE

$$\lim_{k \rightarrow \infty} x(k) = \lim_{z \rightarrow 1} (z-1) X$$

CONVOLUZIONE

DERIVATA

PARABOLA

$$(x * y)(k) = \sum_{i=-\infty}^{+\infty} x(k-i) y(i) \quad \mathcal{L}[x * y] = X \cdot Y$$

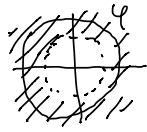
$$-z \frac{dX}{dz} = \mathcal{L}[k x(k)] \quad \mathcal{L}[k^2] = \frac{z(z+1)}{(z-1)^3}$$

ANTITRASF. $\mathbb{Z}$

DOVE ANALITICA

- RE SIGNA
- SVILUPPO FRATTI

$$X(k) = \frac{1}{2\pi j} \oint_{\gamma} X(z) z^{k-1} dz$$



$$\mathcal{L}\left[\binom{k}{h-1} a^{k-(h-1)} 1(k)\right] = \frac{z}{(z-a)^h}$$

$$\Rightarrow x(k) = \sum_i \text{Res} \left\{ X(z) z^{k-1}, p_i \right\}$$

METODO RESIDUI

SINGOLARITÀ
DISTINTE

$$\mathcal{L}\left[\frac{1}{(z-a)^h}\right] = \frac{(k-1)(k-2) \dots (k-h+1)}{(h-1)!} a^{k-h} 1(k-1)$$

... CONTINUA ...

SISTEMI TEMPO DISCRETO

eq. alle differenze

$$f(y(k), y(k-1), \dots, y(k-n)) = g(u(k-n+m), u(\dots), u(k-n))$$

$$\Rightarrow a_n y(k) + a_{n-1} y(k-1) + \dots + a_0 y(k-n) = b_m u(k-n+m) \dots$$

ANALISI SISTEMA

- data eq. alle differenze
- assegnati input e cond. iniziali
- determinare uscita

$$\begin{cases} y(k) \\ y(k-1) \\ \vdots \\ u(k-n+m) \end{cases}$$

TRASFORMAZIONE DI SEGNALE CAMPIONATO

$$y(k) = y_{FOR} + y_{LIB}$$

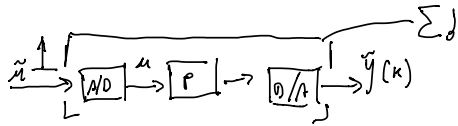
$$y_{FOR} = \mathcal{L}^{-1} \left[\underbrace{\frac{b(z)}{a(z)}}_{\text{FIR}} U(z) \right]$$

$$y_{LIB} = \mathcal{L}^{-1} \left[\underbrace{\frac{c(z)}{a(z)}}_{\text{IIR}} \right]$$

DATA TECN. CONVOLUZIONE

$$y_{FOR}(k) = \sum_i h(k-i) u(i)$$

FUNZIONE TRASF CON DAC



$$\mathcal{Z}[f(t), T] \triangleq \mathcal{Z}[f(kT)] = \mathcal{Z}[f(s), T]$$

RISPOSTA IMPULSO

$$P_d(z) = \mathcal{Z}\left[(1 - e^{-Ts}) \frac{P(s)}{s}, T\right]$$

$$\begin{aligned} \uparrow \\ \Sigma_d &= \frac{z-1}{z} \mathcal{Z}\left[\frac{P(s)}{s}, T\right] \end{aligned}$$

STABILITÀ SISTEMI DISC.

→ sistema Σ_d con fct $H(z)$

- STABILE ↔ poli appartenono a cerchio unitario, molteplicità 1
- ASINT. STABILE ↔ tutti poli interno cerchio unitario
- SEMI-STABILE ↔ almeno un polo su circonf. unitaria, molteplicità 1
- INSTABILE ↔ esterno circ. unitaria

BIBO STABILE

per ogni segnale limitato
risposta limitata

$$\Leftrightarrow \sum_{n=0}^{+\infty} |h(n)| < +\infty$$

$$\Leftrightarrow \text{ASINT. STABILE}$$

DETERMINAZ. STABILITÀ ASINTOTICA

CRITERIO JURY

→ determinare zodi con modulo < 1

→ tutte disuguaglianze soddisfatte

$$\begin{cases} a_n > 0 & n = \text{grado max} \\ (-1)^n a_n > 0 & \text{per } n=2 \rightarrow \text{DIVIDENDO SUFFICIENTE} \\ |a_0| < a_n \\ |b_0| > |b_{n-1}| \\ |c_0| > |c_{n-2}| \\ \vdots \\ |r_0| > |r_1| \end{cases}$$

→ tabella Jury associata a polinomio

	z^0	z^1	z^2	z^3	z^4
1	a_0	a_1	a_2	a_3	a_4
2	a_4	a_3	a_2	a_1	a_0
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→ OMESSI CRITERIO ROUTH, CRITERIO NYQUIST, CRITERIO